Gene Regulation: Lecture 3b July 29, 2009

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Qualitatively Distinct Phenotypes in the Design Space of Biochemical Systems

Outline

- Challenges in relating genotype to phenotype
 - Hierarchy of systems
 - Phenotype of molecular systems?
- Hand-crafted constructions of design space
 - Physiological gene circuits
 - Engineered gene circuits
- Generic constructions of design space
 - Proposal based on the power-law formalism
 - Simple pathway
 - \bullet Core gene circuit for regulation of λ lysogeny
- Summary

"The problems faced by pre- and post-genomic genetics are ... much the same -- they all involve bridging the chasm between genotype and phenotype."

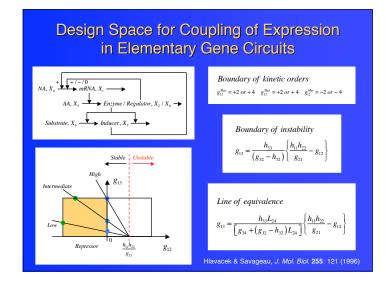
-- Sydney Brenner, Science 287: 2173 (2000).

Three Fundamental Unsolved Problems

- Relationship of the genotype to the molecular components of the organism
 - DNA sequence does not tell what kind of component is being encoded
 - DNA sequence does not tell the *quantitative* values of the parameters
- Relationship of the molecular components to the system that is the organism
 - Parts (and their relevant parameter values) don't tell us how they should fit together
 - Parts don't tell us which of them constitute the system in a given environmental context
- Relationship of the molecular system that is the organism to its phenotypic repertoire
 - System (and the quantitative interaction of all its parts) does not tell us how many qualitatively distinct phenotypes
 - System does not tell us the *relative fitness of the phenotypes*

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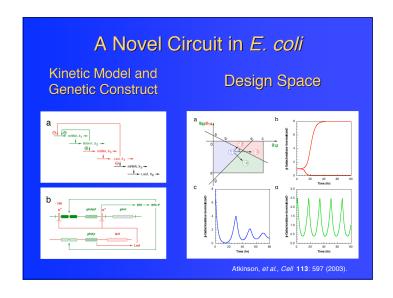
Design Principle for the Coupling of Gene Expression in Elementary Circuits

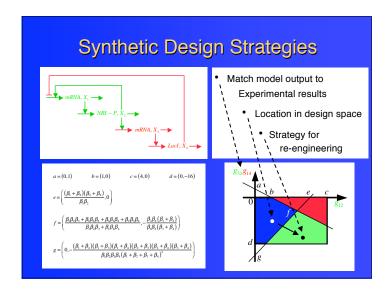
| Mode | Capacity | Predicted coupling |
|----------|----------|---------------------|
| Positive | Small | Inverse & uncoupled |
| Positive | Large | Direct coupled |
| Negative | Small | Direct coupled |
| Negative | Large | Inverse & uncoupled |

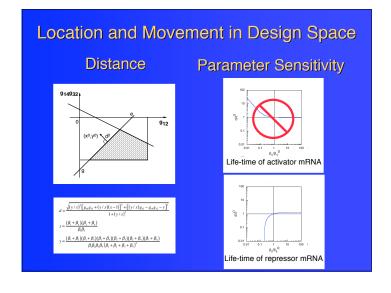
Hlavacek & Savageau, *J. Mol. Biol.* **248**: 739 (1995) Hlavacek & Savageau, *J. Mol. Biol.* **266**: 538 (1997)

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Characteristics of Design Space

- Dimensional *compression* of parameter space
- All parameters included within aggregate factors
- Geometrical relationships
 - Constraints
 - Physical limits
 - Qualitative dynamics
 - Qualitatively distinct functional regimes
- Regions in design space correspond to qualitative distinct phenotypes

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Power-Law Formalism

$$\frac{dX_{i}}{dt} = \sum_{k=1}^{r} \alpha_{ik} \prod_{j=1}^{n} X_{j}^{g_{ik}} - \sum_{k=1}^{r} \beta_{ik} \prod_{j=1}^{n} X_{j}^{h_{ijk}}$$

Canonical from Four Different Perspectives

- Fundamental
- Local
- Piece-wise
- Recast

Savageau, Chaos 11: 142 (2001)

Generic Construction of Design Space

- Model of the system
 - Mass Action representation
 - Rational function representation
 - Other
- Recast into generalized mass action representation
 - Dominant terms produce a piecewise power-law representation
 - Bound on the number of phenotypic regions
- Local performance in each region described by an s-system
 - Signal amplification factors
 - Robustness
 - Response times
- Global performance described by boundaries
 - Regions with qualitative distinct phenotypes
 - Tolerance
 - Design principles

Savageau, et al., PNAS 106: 6435 (2009).

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Two-Step Pathway

Dimensionless equation

$$\frac{dx}{d\tau} = \frac{x_S}{1 + x_S + x/\kappa} - \frac{\rho x}{1 + x + x_P}$$

$$x_S = X_S / K_S$$
 $\kappa = K_I / K$
 $x = X / K$ $\rho = V_{Max,2} / V_{Max,1}$
 $x_P = X_P / K_P$ $\tau = (V_{Max,1} / K)t$

Steady-state equation

$$\frac{x_S}{1 + x_S + x / \kappa} = \frac{\rho x}{1 + x + x_P}$$

Recast equation

 $X_s \rightleftharpoons X \rightleftharpoons X_p$

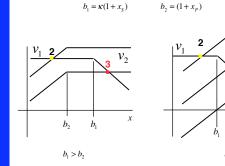
$$x_{s}x_{2}^{-1} = \rho x_{1}x_{3}^{-1}$$

 $x_{2} = (1 + x_{s}) + x_{1} / \kappa$
 $x_{3} = (1 + x_{p}) + x_{1}$

Bounds on # of regimes

$$T \le \prod_{i=1}^{n} P_i * N_i = 1 * 2 * 2 = 4$$

Steady-State Solutions for *x*: Three Qualitatively Distinct Cases



Piecewise Representation

$$\frac{dx}{d\tau} = \frac{x_S}{1 + x_S + x/\kappa} - \frac{\rho x}{1 + x + x_P}$$

$$X_s \stackrel{\mathbf{v_1}}{\rightleftharpoons} X \stackrel{\mathbf{v_2}}{\rightleftharpoons} X_p$$

$$\left[\frac{\kappa(1+x_P)x_S}{\rho}\right]^{1/2}$$

$$x > \kappa(1 + x_S) \quad x < (1 + x_P)$$

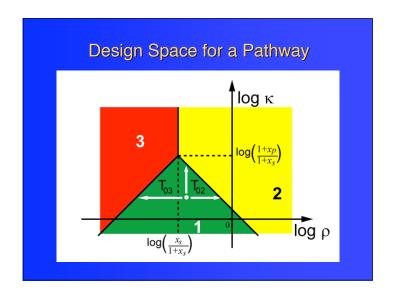
$$\frac{x_s(1+x_p)}{\rho(1+x_s)}$$

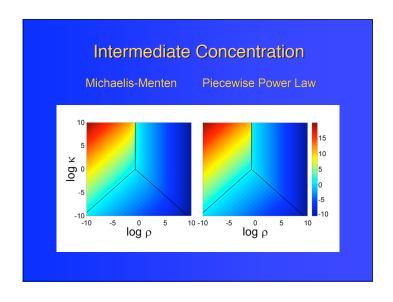
$$x < \kappa(1+x_s) \quad x < (1+x_p)$$

$$\frac{\kappa x_s}{2}$$

$$x > \kappa(1 + x_s) \quad x > (1 + x_p)$$

$$x < \kappa(1+x_s) \quad x > (1+x_p)$$





Design Principle

$$X_s \stackrel{\mathbf{v_1}}{\longleftarrow} X \stackrel{\mathbf{v_2}}{\longleftarrow} X_p$$

Monofunctional

$$\frac{(1+x_p)x_S}{\kappa(1+x_S)^2} > \rho > \frac{\kappa x_S}{(1+x_p)}$$

Bifunctional

$$\begin{aligned} \frac{(1+x_p)}{\kappa(1+x_s)} > 1 & \rho > \frac{(1+x_p)x_s}{\kappa(1+x_s)^2} \\ or & \\ \frac{(1+x_p)}{\kappa(1+x_s)} < 1 & \rho > \frac{x_s}{(1+x_s)} \end{aligned}$$

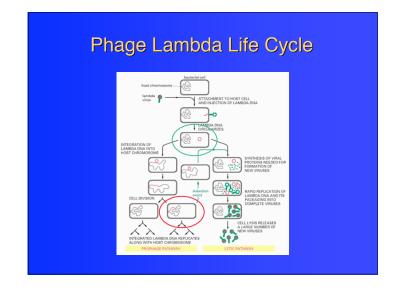
 κ small and ρ large

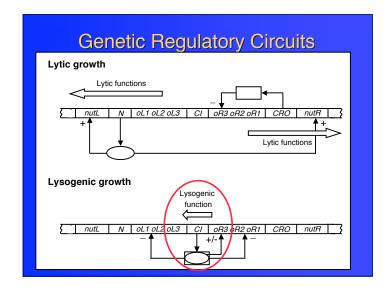
Implications

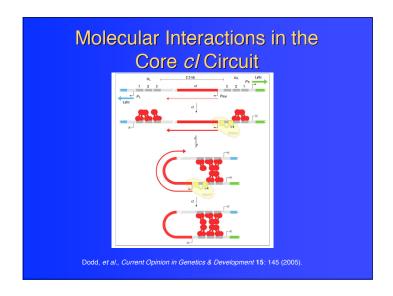
- 9-D parameter space compressed to 2-D design space
- Analysis within regimes is greatly simplified
- Phenotype of regime most appropriate for a "monofunctional" intermediate
 - Minimal accumulation of intermediate avoids toxicity
 - Fast response time
 - Locally robust to changes in parameters
- Phenotype of regime 2 most appropriate for a "bi-functional" intermediate
 - Accumulation of intermediate facilitates functioning as a metabolic signal
 - Greater gain in flux when responding to input signals
- Phenotype of regime 3 has no appropriate function
- Global tolerance precisely defined as the parameter change necessary to cross the nearest boundary

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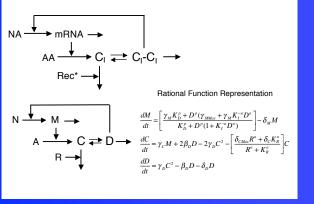




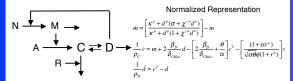


Model Formulation



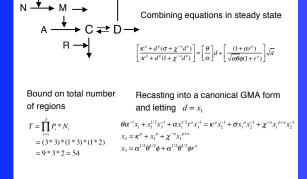


Normalized Equations

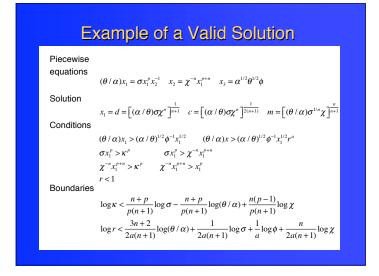


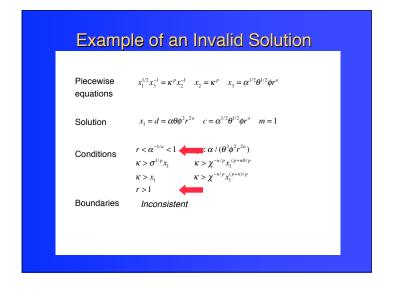
Normalized variables about steady state with maximal induction
$$\begin{split} \phi &= \left(\frac{\gamma_M \gamma_C \gamma_D}{2 \delta_M \delta_D (\beta_D + \delta_D)}\right)^{1/2} \quad r = \frac{1}{K_R} R \qquad \sigma = \frac{\gamma_{MMax}}{\gamma_M} \qquad \rho_C = \sqrt{\alpha \theta} \phi \frac{\delta_C}{\delta_M} \\ m &= \frac{\delta_M}{\gamma_M} M \qquad \qquad \kappa = \frac{\delta_M \delta_C}{\gamma_M \gamma_C} \alpha K_D \qquad \alpha = \frac{\delta_{CMax}}{\delta_C} \qquad \rho_D = \frac{\beta_D + \delta_D}{\delta_M} \\ c &= \frac{\delta_M \delta_C}{\gamma_M \gamma_C} \sqrt{\alpha \theta} \phi C \qquad \qquad \chi = \frac{\delta_M \delta_C}{\gamma_M \gamma_C} \alpha K_I \qquad \theta = \frac{2\delta_D}{\delta_C} \qquad \tau = \delta_M t \\ d &= \frac{\delta_M \delta_C}{\gamma_M \gamma_C} \alpha D \qquad \chi = \frac{\delta_M \delta_C}{\gamma_M \gamma_C} \alpha K_I \qquad \theta = \frac{2\delta_D}{\delta_C} \qquad \tau = \delta_M t \end{split}$$

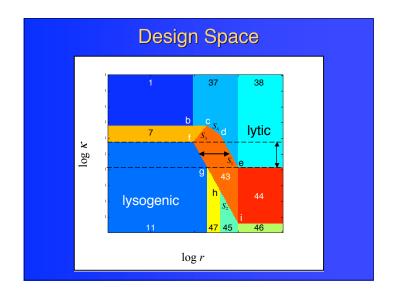
Recast Steady-State Equations



Construction of System Design Space







Landmarks in Design Space I

Intersections

$$b = \frac{1}{a}\log(\theta/\alpha) + \frac{1}{a}\log\phi, \frac{n+p}{p(n+1)}\log\sigma - \frac{n+p}{p(n+1)}\log(\theta/\alpha) + \frac{n(p-1)}{p(n+1)}\log\chi$$

$$\begin{split} c &= \frac{3n+2}{2a(n+1)}\log(\theta/\alpha) + \frac{1}{2a(n+1)}\log\sigma + \frac{1}{a}\log\phi + \frac{n}{2a(n+1)}\log\chi, \\ &\frac{n+p}{p(n+1)}\log\sigma - \frac{n+p}{p(n+1)}\log(\theta/\alpha) + \frac{n(p-1)}{p(n+1)}\log\chi \end{split}$$

$$d = \frac{1}{2a}\log(\theta/\alpha) + \frac{1}{a}\log\sigma + \frac{1}{a}\log\phi - \frac{1}{2a}\log\chi,\log\chi$$

$$e = 0, 2\log \sigma + 2\log \phi + \log(\theta/\alpha)$$

Location in System Design Space

Landmarks in Design Space II

$$f = \frac{1}{a}\log(\theta/\alpha) + \frac{1}{a}\log\phi, \frac{1}{p}\log\sigma - \log(\theta/\alpha)$$

$$\begin{split} g &= \frac{3n+2}{2a(n+1)}\log(\theta/\alpha) + \frac{1}{2a(n+1)}\log\sigma + \frac{1}{a}\log\phi + \frac{n}{2a(n+1)}\log\chi, \\ &\frac{n+1-p}{p(n+1)}\log\sigma - \frac{2n+1}{(n+1)}\log(\theta/\alpha) - \frac{n}{(n+1)}\log\chi \end{split}$$

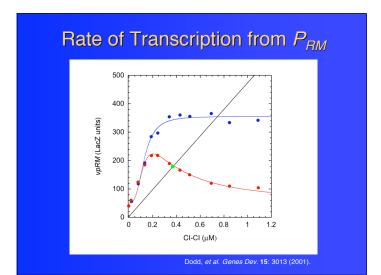
$$h = \frac{1}{2a}\log(\theta/\alpha) + \frac{1}{a}\log\sigma + \frac{1}{a}\log\phi - \frac{1}{2a}\log\chi, \log\chi - \frac{2p-1}{p}\log\sigma$$

$$i = 0, \frac{1}{p}\log \sigma + \log(\theta/\alpha) + 2\log$$

Slopes
$$s_1 = s_2 = -2a$$

$$s_3 = \frac{2a(p-1)}{p}$$

Slopes
$$s_1 = s_2 = -2a$$
 $s_3 = \frac{2a(p-1)}{p}$ $s_4 = -\frac{2a(p+n)}{p(2n+1)}$



Parameters Values From **Experimental Data**

Fitting model to data without inhibition

 Capacity for regulation by CI Normalized K_M for activation Hill number for activation p=3

Fitting model to data with inhibition

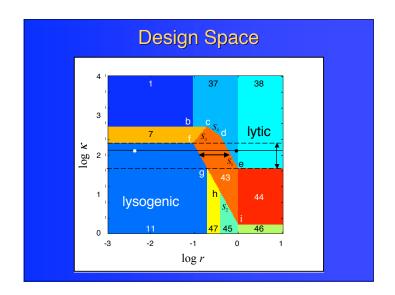
 Normalized K₁ for repression $\chi = 230$

Hill number for repression

Fitting model to the normal operating point in

 Capacity for regulation by RecA* α=215 φ=10

Parameter characterizing dimerization of CI



Evaluation of Local Behavior

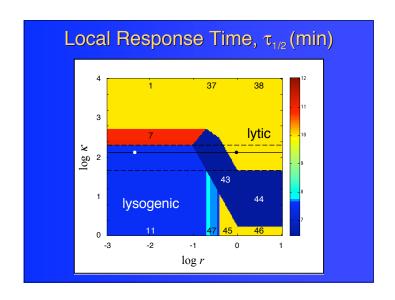
Local Criteria for Functional Effectiveness $Min\left[\sum |S(D,p_i)|\right]$ 1. Maximize local robustness of D to parameter 2. Minimize response in D to variations in R $Min \left[\sum |S[L(D,R),p_i]| \right]$ 3. Maximize local robustness of L(D,R) to parameter 4. Minimize response in M to variations in R $Min\ L(M,R)$ $Min \left[\sum |S[L(M,R),p_i]| \right]$ 5. Maximize local robustness of L(M,R) to parameter variation 6. Minimize response time $Min \left| \text{Re} \left[\lambda_{domnant} \right]^{-1} \right|$ 7. Maximize local robustness of λ to parameter variation $Min\left[\sum |S[Re(\lambda)^{-1}, p_i]|\right]$

Local Robustness in Each Phenotypic Region

| Region | Criteria | | | | | |
|------------|-------------------|-------------------|-------|-------------|-------|------------|
| | L1 | L2 | L3 | L4 | L5 | L6 |
| Lysogenie | regions (stable | steady states) | | | | |
| 11 | 0.161±0.209* | 0.222±0.282 | 0.000 | 0.000 | 0.000 | 0.000 |
| 47 | 0.209±0.248 | 0.293±0.267 | 0.500 | 0.117±0.301 | 0.750 | 0.088±0.28 |
| 45 | 0.862±0.878 | 0.133±0.340 | 2.000 | 0.067±0.249 | 0.000 | 0.000 |
| 46 | 0.667±0.863 | 0.133±0.340 | 0.000 | 0.000 | 0.000 | 0.000 |
| Hysteretic | regions (unstab | le steady state s |) | | | |
| 7 | 0.277±0.410 | 0.474±0.657 | 0.000 | 0.000 | 0.000 | 0.000 |
| 43 | 0.323±0.325 | 0.555±0.497 | 0.400 | 0.147±0.376 | 1.200 | 0.077±0.27 |
| 44 | 0.230±0.308 | 0.381±0.433 | 0.000 | 0.000 | 0.000 | 0.000 |
| Lytic regi | ons (stable stead | y states) | | | | |
| 1 | 0.267±0.442 | 0.133±0.340 | 0.000 | 0.000 | 0.000 | 0.000 |
| 37 | 0.862±0.878 | 0.133±0.340 | 2.000 | 0.067±0.249 | 0.000 | 0.000 |
| 38 | 0.667±0.863 | 0.133±0.340 | 0.000 | 0.000 | 0.000 | 0.000 |

^{*} Mean ± standard deviation

Evaluation of Global Behavior



Global Criteria for Functional Effectiveness

| 4 Marrianian | accidedates a secu | and Alam Income | madia na sia. | |
|--------------|--------------------|-----------------|---------------|--|

2. Maximize robustness of this operation

3. Maximize hysteretic buffer

4. Maximize robustness of buffer

5. Maximize switching speed

6. Maximize Robustness of switching speed

7. Maximize global tolerances in best phenotypic region

 $Max \Delta_S = \alpha^2 / \left[\theta^2 \phi^2 \sigma^{(2p-1)/p} \right]$

 $Max \left[\sum_{i} \left| S(\Delta_{S}, p_{i}) \right| \right]^{-1}$

 $Max \Delta_n = \sigma^{[(2p-1)/(2pa)]}$

 $Max \left[\sum |S(\Delta_H, p_i)| \right]$

 $Max \tau_s^{-1}$

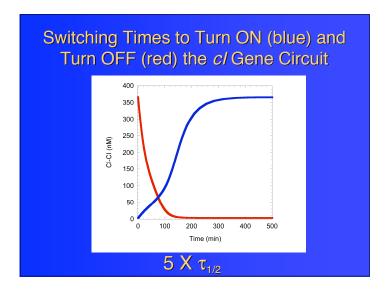
 $Max \left[\sum_{i} \left| S(\tau_{S}, p_{i}) \right| \right]$

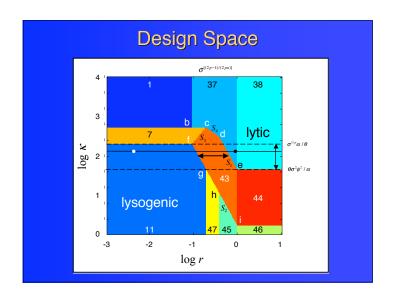
 $Max[T_{low},T_{high}]$

Global Tolerances for the Lysogenic Phenotype

| mR | mRNA | | Protein | | |
|---------------------------------|------------|---------------------------------|------------|--|--|
| Parameter | Tolerance | Parameter | Tolerance | | |
| $\gamma_{\scriptscriptstyle M}$ | [∞,4.2]* | δ_c | [∞,4.2] | | |
| $\gamma_{M{ m max}}$ | [2.4,1.7] | $\delta_{_{C\mathrm{max}}}$ | [1.6, 38] | | |
| K_D | [2.8, 4.1] | K_R | [38,∞] | | |
| K_I | [11,2.4] | R | [∞, 38] | | |
| p | [∞,∞] | а | [4.8,∞] | | |
| n | [∞,∞] | γ_c | [2.4,1.7] | | |
| $\delta_{\scriptscriptstyle M}$ | [1.7,2.4] | $\gamma_{\scriptscriptstyle D}$ | [∞,2.8] | | |
| $\delta_{\scriptscriptstyle D}$ | [11,2.1] | $\beta_{\scriptscriptstyle D}$ | [2.8,1500] | | |

* [fold decrease,fold increase]





Additional Influences on the Core *cl* Circuit

- Effects promoting induction (Atsumi & Little, 2006)
 - CRO is unnecessary for induction (Svenningsen, et al., 2005).
 - But it does lower the maximal rate of cl transcription γ_{IMmax}, which reduces the threshold level of RecA* needed for induction
- Effects promoting lysogeny (Kourilsky & Knapp, 1974)
 - Multiplicity of infection leads to elevated CII levels (Kobiler, et al., 2005)
 - This increases the maximal rate of cl transcription $\gamma_{
 m Mmax}$
 - Thus, raising the boundary between the lytic and lysogenic regions
 - Slower growth rates lead to an increase in CI
 - This is a result of lowering the rate constant for dilution δ_c
 - Again, expanding the lysogenic regions at the expense of the lytic regions

Implications

- 15-D parameter space compressed to 2-D design space
- Analysis within regimes is greatly simplified
- Phenotypes representing the stable steady state with induction
- Phenotypes representing multiple steady states with an hysteretic response
- Phenotypes representing less appropriate steady states for the lysogenic state.
- Phenotypes representing most appropriate steady state for the lysogen
 - Locally robust to parameter changes
 - Fast response times
 - Large global tolerance to parameter changes
 - Fast switching times for induction and integration
- Qualitative prediction of hysteretic region
- Suggestions for design principles
 - Δ;
 - . .
 - Cleavage only of the monomer
 - Induction much faster then integration

Summary

- Motivated by results from successful hand-crafted design spaces
- Proposal for a generic method of constructing design space
 - Design space as a dimensional compression of parameter space
 - Phenotypes associated with regions of design space
 - Bound on the number of qualitatively distinct phenotypes
 - Simple characterization of local behavior within regions
 - Fitness comparisons among phenotypes
 - Precisely defined boundaries between regions
 - Novel definition of **global tolerance** to parameter change
 - Facilitates identification of system design principles
- Foundation in algebraic geometry
 - All boundaries are straight lines in log space
 - Intercepts are linear in the logarithms of the rate constants
 - Slopes and intercepts are rational functions of the kinetic orders

Acknowledgements

- Eberhard Voit
- William Hlavacek
- Armindo Salvador
- Pedro Coelho
- Dean Tolla
- Rick Fasani

• NIH, NSF, ONR